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Technical Report

No. 13504

M915 Radiator Reverse Engineering Effort
SEPTEMBER 1990

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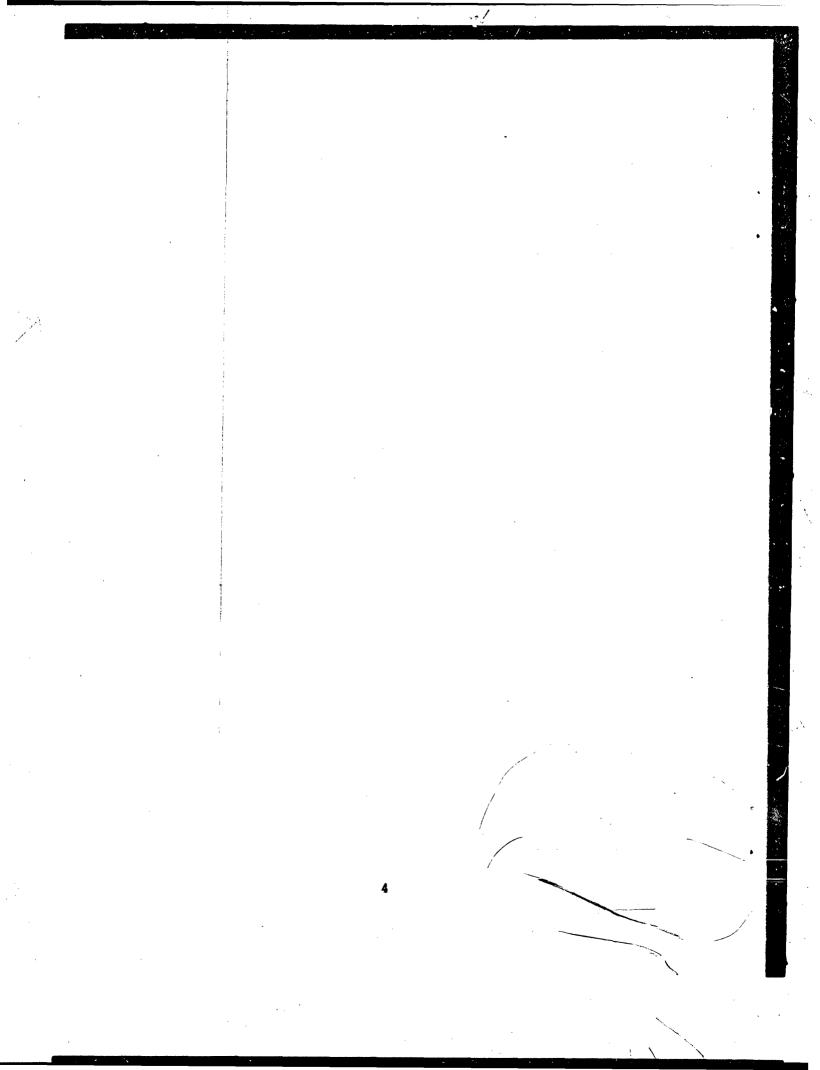
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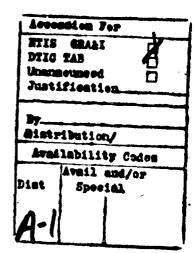
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1.0. INTRODUCTION

This report describes the cooling test program of the M915 tractor truck radiator which was conducted to develop the performance requirements needed for competitive procurement. The test requirements and report were developed by the Transmissions and Integration Branch of the Propulsion Systems Division, U.S. Army Tank-Automotive Command (TACOM).

2.0. OBJECTIVE

The primary objective of this program was to conduct cooling performance testing of two new radiators to develop performance requirements for inclusion onto a level-3 drawing to be used for competitive procurement.

3.0. CONCLUSIONS

3.1. The heat rejection for the power pack is approximately 10,650 BTU/min (10,250 BTU/min for engine, 400 BTU/min for transmission and other components) (see Appendix A). This radiator was able to meet the cooling requirement for each test run, based on test derivation from MIL-R-45306C.

4.0. RECOMMENDATIONS

- 4.1. Use the test data as performance criteria and combine with other standard radiator requirements for incorporation into a M915 radiator level-3 drawing (see Appendix B).
- 4.2. Perform similar testing on all other military radiators without government-owned TDPs to develop individual radiator performance requirements. This would preclude shortage problems arising from sole-source acquisition.
- 4.3. Establish an improved quality inspection procedure for the radiators either at the manufacturer's facilities or upon arrival at Army depots.

5.0. DISCUSSION

5.1. Background

The lack of radiators in the Army Supply System and the delays in delivery from the sole-source supplier created a need to investigate additional sources. In order to solicit additional sources, radiator performance requirements were needed. The absence of a government-owned Technical Data Package (TDP) brought about this investigation to develop performance requirements for the subject radiator.

The performance testing was conducted at TACOM's Air Flow Laboratory from April 1990 through May 1990.

5.2. Scope and Limitations

The unavailability of radiators in the Army Supply System limited the amount of samples to be used for testing. The two test radiators were received from the depot's latest shipment of newly produced radiators delivered by the manufacturer. The scope of this report will cover the testing that was performed and the development of performance requirements for the M915 radiator.

5.3. Outline of Test

The test program consisted of the following operations:

Determination of cooling requirements.

Development of check-out procedures and performance tests.

Installation and instrumentation of radiator.

Collection of test data.

Cleaning and preparation of radiator for return shipment.

Evaluation and reporting of test results.

5.4. Test Material and Equipment

Two (2) M915 radiators, NSN 2930-01-082-7922, were obtained from the manufacturer and were used in this test program.

TACOM's Air Flow Laboratory and associated equipment and instrumentation were used to perform the testing. During heat-rejection testing, 18 thermocouples were gridded and placed on each side of the radiator core to measure the average inlet and outlet air temperatures. Quartz thermometers were used to measure the inlet and outlet water temperatures.

5.5. Test Procedures

As no test procedure was available for this radiator, MIL-R-45306C, "Radiators, Engine Cooling, Industrial" (see Appendix A) was used to derive test points for the heat-rejection data. Additional tests such as the fill-rate test, maximum free-flow rate test, and pressure-cap test were included in the test plan and were performed to provide additional radiator performance data. These tests were obtained from the TACOM Cooling System Design Guide. Testing of the radiators was conducted in various steps to insure proper accuracy and to determine radiator characteristics. The details of these steps are described below:

- 5.5.1. Visual Inspection of Radiators. Visual inspection was performed to document any noticeable external defects.
- 5.5.2. Preliminary Water-Pressure Test. With all ports blocked, the radiator was completely filled with water and pressurized to 20 psig. The radiator was then checked for leakage, and results were recorded.
- 5.5.3. Air-Pressure Test. An air hose was connected to the radiator and with all ports blocked, was pressurized to 20 psig. The radiator was then submerged in a reservoir of water and was inspected for air leaks. Results were recorded.
- 5.5.4. Flushing of Radiators. The radiators were thoroughly flushed with water until a clean fluid was seen exiting the radiator. This was done to ensure that no deposits would be present during testing of the cooling system.
- 5.5.5. Fill-Rate Test. With the outlet port blocked, the radiator was filled to 90 percent capacity, and the fill time was recorded. This procedure was conducted to ensure that a five-minute time limit was met.
- 5.5.6. Maximum Free-Flow Rate Test. The radiator was suspended below a receiving drum and connected to a water flow system. The water was adjusted so that a constant water level of one-half inch above inlet port of the radiator was maintained. Flow measurements were recorded to determine the maximum free-flow rate of the radiator (see figure 5-1).
- 5.5.7. Pressure-Cap Test. A standard pressure-cap testing device was used to measure the relief valve setting of the cap.
- 5.5.8. Heat-Transfer and Core-Resistance Tests. The radiator was mounted in a wind tunnel and was tested at 190, 195, and 125 percent of the rated coolant flow specified in MIL-R-45396C. At each coolant-flow rate, the heat rejection was determined at the following air velocities:

COOLANT FLOW RATE (OPM)	AIR VELOCITY
110	1600 1800 2100
116	1600 1800 2100
186	1600 1800 2100

TABLE 5.1 HEAT-TRANSFER TEST CONDITIONS

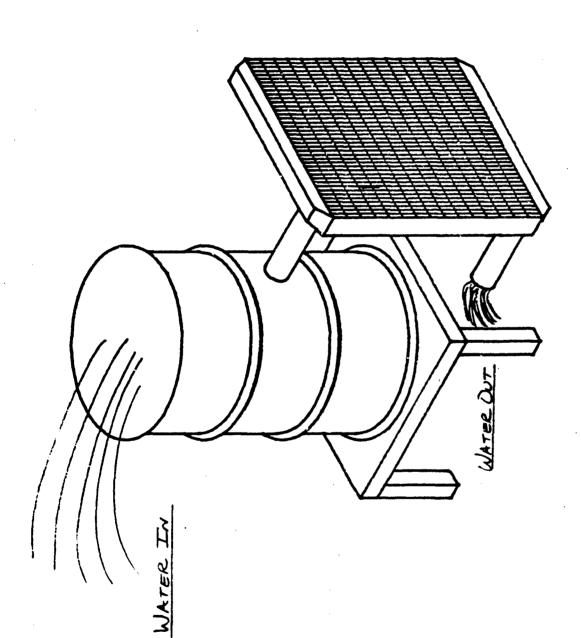


Figure 5-1. Maximum Free-Flow Rate Test Set-Up

Heat rejection was calculated according to the following equations:

A. Heat Transfer - Heat energy absorbed by air flow:

Where m = Air flow rate (lbm/minute)

Cp = Specific heat of air (Btu/lbm/F)

LT = Air Temperature Difference (F)

B. Heat Transfer - Heat rejection from coolant flow:

Where m = Coolant flow rate (lbm/minute)

Cp = Specific heat of coolant (BTU/lbcc/F)

LT = Coolant Temperature Difference (°F)

5.5.9. Final Air-Pressure Test. The Preliminary Air-Pressure Test was repeated to ensure that no damage was made to the radiators during testing.

5.6. Radiator Configuration

The current configuration of the M915 radiators are crossflow heat exchangers with uninterrupted plain-fin surfaces (see figure 5-2). The core area is approximately 1200 square inches, and the coolant capacity is 17.25 gallons.

5.7. Test Results

The following paragraphs summarize the results of each test that was performed. For more detailed tabulated results, see Appendix B.

- 5.7.1. Visual Inspection of Radiators. Portions of the core were missing near both the top and bottom tanks on both radiators. Figures 5-3 and 5-4 show these deficiencies. Prior to start of the Preliminary Water-Pressure Test, a thick yellow fluid was found inside sample \$1. When the radiator was filled with water, this fluid floated to the top of the water. In sample \$2, before filling the radiator with water, a yellowish brown fluid was found. Chemical analysis revealed that the characteristics appeared to be similar to those of a transmission oil fluid. A detailed test report of this analysis can be found in Appendix B. No military specifications call for a preservative oil to be placed inside the radiator, however, the manufacturer could have placed the fluid on his own accord. These fluids were removed, and the radiators were flushed clean before proceeding with the test.
- 5.7.2. Preliminary Water-Pressure Test. No leakage occurred in either of the two radiator test samples.
- 5.7.3. Air-Pressure Test. A small leak was noticed on radiator sample #1 from a bolt located below the radiator outlet on the lower tank. After the radiator was submerged for 30 minutes, the leak stopped.

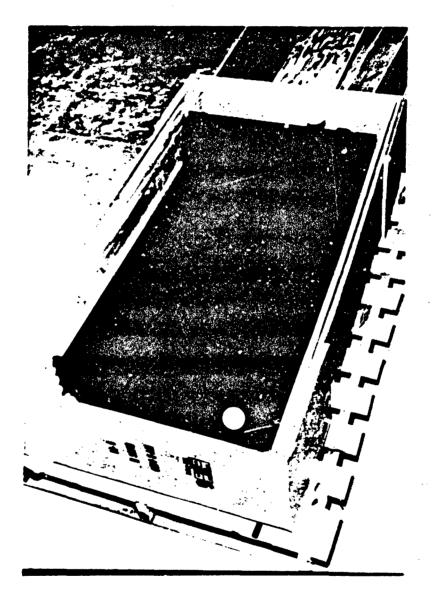


Figure 5-2. M915 Radiator Configuration



Figure 5-3. Radiator Quality Deficiencies, Test Sample #1

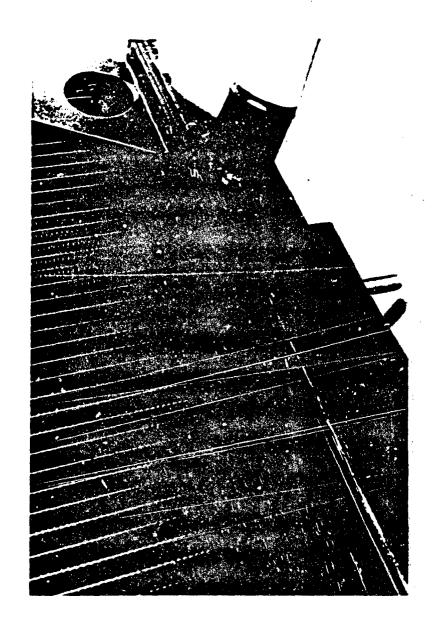


Figure 5-4. Radiator Quality Deficiencies, Test Sample #2

On radiator sample #2, a small leak was initially cited at the soldering joint between the fillerneck and the top tank. This leak gradually became worse and, upon stabilization, was measured at 21,660 ml/min (5.722 GPM).

- 5.7.4. Flushing of Radiators. Both test radiators were flushed out with water to ensure that clean cooling systems would be used during the heat transfer test. During flushing, clean water was observed leaving both radiators.
- 5.7.5. Fill Rate Test. In order to fill the radiator to 90 percent capacity, an average fill rate of 0.29 minutes was recorded by both radiators.
- 5.7.6. Maximum Free-Flow Rate Test. After coolant flow was stabilized, an average measurement of 52.8 GPM was recorded for radiator sample #1 and 57.7 GPM was recorded for radiator sample #2. Combining test runs from both radiators produced an average maximum free-flow rate of 55.3 GPM.
- 5.7.7. Pressure-Cap Test. The pressure caps of both radiator samples were tested and measured 9.9 psi and 10 psi, respectively.
- 5.7.8. Heat-Transfer and Core-Resistance Tests. Four test runs, out of a total of 18, were removed from the final analysis. These four runs did not meet the 5 percent-difference specification between air heat rejection and coolant heat rejection. Test data showed that the radiator met the cooling requirements of the vehicle's powerpack.
- 5.7.9. Final Pressure Test. Radiator sample #1 did not show any signs of leakage. Radiator sample #2 had repairs on the fillerneck but still maintained a small leak. This leak was measured to be approximately 997 ml/min (9.263 GPM).

5.8. Discussion of Results

The resulting core-resistance data may look suspicious, as it does not agree with those values found in MIL-R-45306C. It therefore must be reiterated that this specification was used solely as a test parameter design guide, and not as a performance guide. The resulting core-resistance data derived from this testing did provide adequate cooling. If restriction on the radiators were too great, then the cooling requirements of this radiator's cooling system would which likely not have been met. The results of the heat-transfer testing proved that this vehicle's cooling requirements were met by this radiator design.

5.9. Other

Vibration and pressure—cycle tests were not included in this test plan. These tests are destructive tests, and the radiator samples that were used during testing were on loan to TACOM. These tests are also known as structural tests, not performance tests, and the purpose of the testing was to determine performance requirements.

APPENDIX A

M915 RADIATOR TEST REQUIREMENTS DATA

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All data is based on the engine operating with fuel system, weter pump, lubricating oil pump, compressor (unloaded) and air cleaner; not included are atternator, fan, optional equipment and driven components. Data is based on uperation under SAE standard 3816b conditions of 500 feet (150 m) attitude (29.00 in. {736 mm} Hg dry becometer), 85°F (29°C) intake air temperature and 0.38 in. (9.6 mm) Hg weter vapor pressure, using No. 2 diesel or a fuel corresponding to ASTM D2.

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MIL-R-45306C 3 May 1983 SUPERSEDING MIL-R-45306B 3 July 1973

HILITARY SPECIFICATION

RADIATORS, ENGINE COOLING, INDUSTRIAL

This specification is approved for use by all Departments and Agencies of the Department of Defense.

1. SCOPE

- 1.1 Scope. This specification covers coolant radiators for liquid-cooled, industrial, internal-combustion engines of 10 horsepower and above.
- 1.2 Classification. The radiators shall be of the following types, as specified (see 6.2):

Type I - Soldered-tank radiator.

Type II - Bolted-tank radiator with replaceable core.

2. APPLICABLE DOCUMENTS

2.1 Government documents.

2.1.1 Specifications and standards. Unless otherwise specified (see 6.2), the following specifications and standards of the issue listed in that issue of the Department of Defense Index of Specifications and Standards (DoDISS) specified in the solicitation, form a part of this specification to the extent specified herein.

SPECIFICATIONS

FEDERAL

VV-L-800

- Lubrication Oil, General Purpose, Preservative (Water-Displacing, Low Temperature).

Beneficial comments (recommendations, additions, deletions) and any pertinent data which may be of use in improving this document should be addressed to: US Army Mobility Equipment Research and Development Command, ATTN: DRDME-DS, Fort Belvoir, VA 22060 by using the self-addressed Standardization Document Improvement Proposal (DD Form 1426) appearing at the end of this document or by letter.

MTL-R-45304C

· •	•	
PPP-3-601		- Boxes, Wood, Cleated-Plywood.
PPP-8-636		- Boxes, Shipping, Fiberboard.
HILITARY		The state of the s
MIL-P-116	•	- Preservation, Methods of.
MTL-C-5501	•	- Con and Ding Protective Due

STANDARUS

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MIL-G-12803

MIL-T-22085

•	
MIL-STD-105	- Sampling Procedures and Tables for
•	Inspection by Attributes.
MIL-STD-129	- Marking for Shipment and Storage.
MIL-STD-130	Identification Marking of US
	Hilitary. Property.
MIL-STD-889	- Dissimilar Metals.
MIL-STD-1188	- Commercial Packaging of Supplies
•	and Iquipment.
MS35773	- Radiators, Engine Cooling, Industrial.
M535884	- Cores, Radiators, Engine Cooling,

Seal.

Gasket Material, Monmetallic.

Preservation and Sealing

Industrial.

Tape, Pressure-Sensitive, Adbesive,

. (Copies of specifications, and standards required by contractors in connection with specific acquisition functions should be obtained from the contracting activity or as directed by the contracting officer.)

2.2 Other publications. The following document(s) form a part of this specification to the extent specified herein. The issues of the documents which are indicated as DoD adopted shall be the issue listed in the current DoDISS and the supplement thereto, if applicable.

AMERICAN NATIONAL STANDARDS INSTITUTE (AMSI)

AMSI/ASTM B-36 - Brass Plate, Sheet, Strip, and Rolled Bar. AMSI/ASTM B-152 - Copper Sheet, Strip, Plate, and Rolled Bar.

(Application for copies should be addressed to the American Mational Standards ... Institute, Inc., 1430 Broadway, New York, NY 10018).

AMERICAN SOCIETY FOR TESTING AND NATERIALS (ASTM)

A308 - Twine Plates.

(Application for copies should be addressed to the American Society for Testing and Materials, 1916 Race Street, Philadelphia, PA 19103.)

(Industry association specifications and standards are generally available for reference from libraries. They are also distributed among technical groups and using Federal agencies.)

2.3 Order of precedence. In the event of a conflict between the text of this specification and the references cited herein, the text of this specification shall take precedence.

3. REQUIREMENTS

- 3.1 <u>Description</u>. The radiators and cores shall be as shown on MS35773, MS35884, and as specified herein.
- 3.2 First article (first-produced radiator and core). The contractor shall furnish one or more radiators and cores as specified (see 6.2), for examination and tests within the time frame specified (see 6.2), to prove prior to starting production, that, his production methods will produce radiators and cores that comply with the requirements of this specification. Examination and tests shall be as specified in Section 4 and upless otherwise specified herein, all examination and tests shall be conducted by the contractor subject to surveillance and approval by the Government (see 6.3). When specified (see 6.2), the Government will conduct any or all of the preproduction examination and tests.
 - 3.3 Materials. Materials shall be as specified herein and as shown on applicable standards. Materials not specified shall be selected by the contractor and shall be subject to all provisions of this specification (see 6.5).
 - 3.3.1 Copper tubing. Tubes shall be copper, red brass, or naval brass with 85 percent copper and 15 percent zinc. Tubing shall not be subject to dezincification and resultant corrosion.
 - 3.3.2 Sheet copper. Sheet copper for fins shall conform to ANSI/ASTM B152.
 - 3.3.3 Sheet brass. Sheet brass for tanks and header plates shall conform to ANSI/ASTM B36.
 - 3.3.4 Terne plate. Terne plate for side members for type I radiators shall conform to ASTM A308 Terne Plate, with LT-35 coating thickness as a minimum.
 - 3.3.5 Gasket. Gasket material shall conform to MIL-G-12803, Type I, identification number P1161A.
 - 3.3.6 <u>Dissimilar Metals</u>. Dissimilar metals as defined in MIL-STD-889 shall not be used in intimate contact without suitable protection in order to prevent or minimize galvanic corrosion.
 - 3.3.7 Identification of materials and finishes. The contractor shall identify the specific material, material finish, or treatment for use with components and subcomponents. This information shall be available, upon request, to the contacting officer or his or her designated representative.

- 3.3.8 Material deterioration and control. The radiators shall be fabricated from compatible materials, inherently corrosion resistant or treated to provide protection against the various forms of corrosion and deterioration that may be encountered in any of the applicable storage and operating environments to which the item may be exposed.
 - 3.4 Fins and tubes. The core assembly shall be of the tube and plate-fin construction with the fins perpendicular to and in close contact with the tubes.
 - 3.5 Performance.
- 3.5.1. Heat rejection and core resistance. The heat rejection and core resistance curves of the test core shall be compared with the corresponding heat rejection and core resistance curves of the standard core. A fan curve at standard air density (0.075 lbs/cu. ft.) shall be drawn through the standard core resistance points at the 1500, 1800 and 2100 feet per minute air velocity points. The point at which the fan curve intersects the test core resistance curve shall be projected onto its respective heat rejection curve. When compared to the standard core values, the projected core values shall conform to the values stated on sheet A of MS35773.
 - 3.5.2 Heat rejection comparison. The comparison between heat rejection (air gain) and heat rejection (water loss) shall not exceed 5 percent.
 - 3.5.3 Distortion. When tested as specified in 4.5.2.3, the radiator and core shall show no leakage or permanent distortion exceeding 1/8 inch.
- 3.5.4 Vibration and leakage. The radiator or core when vibrated as specified in 4.5.2.4 at the most critical resonant frequency shall show no evidence of structural damage, seepage, or leakage.
 - 3.6 Identification marking. Radiators and type II cores shall be identified in accordance with HIL-STD-130. A metal identification plate shall be permanently affixed to the side of the top tank of each radiator near the water inlet. In addition, a metal identification plate shall be permanently attached to the side of the type II core. Marking shall include the following information

Military standard radiator

MS part number
Hanufacturer's name or trademark

- 3.7 Finishing and painting. Unless otherwise specified (see 6.2), the rediator and core shall be finished and painted in accordance with the contractor's standard practice.
 - 3.8 Type I. The type I soldered-tank radiator shall be as shown on MS35773, part numbers -1, -2, -3, -9 or -10, as specified (see 6.2).
 - 3.9 Type II. Bolted-tank radiator with replaceable core, type II, shall be as shown on MS 35773, part numbers -4, -5, -6, -7, or -8, as specified (see 6.2).

3.10 Workmanship.

- 3.10.1 Cleaning. The completed radiator and cores shall be cleaned and free from defects such as dirt, sand, metal chips, rust, cracks, and other foreign materials or defects that could impair their serviceability. Water from the cleaned radiator or cores shall not show a "pH" change of greater than 1, the chloride content shall not exceed 75 parts per million, nor shall there be a change in chlorine content no greater than 75 parts per million when compared with water before rinsing.
- 3.10.2 Soldering. Soldering of the overflow tube to the filler neck and the filler neck to the radiator top tank shall not interfere with the proper operation of the pressure cap. In the event any soldering is done to parts after the radiator or core has been cleaned, the radiator or core shall be cleaned again after the soldering operation.
- 3.10.3 Reader plates. The gasket area, the corresponding boltholes, and the bolthead area of the header plates used on type II radiators shall be free of solder lumps and a water resistant nonhardening cement shall be used on the gaskets when the core is assembled to the tanks.

4. QUALITY ASSURANCE PROVISIONS

CANADA CONTRACTOR SERVICE

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- 4.1 Responsibility for inspection. Unless otherwise specified in the contract or purchase order, the contractor is responsible for the performance of all inspection requirements as specified herein. Except as otherwise specified in the contract or order, the contractor may use his own or any other facilities suitable for the performance of the inspection requirements specified herein, unless disapproved by the Government. The Government reserves the right to perform any of the inspections set forth in the specification where such inspections are deemed necessary to assure supplies and services conform to prescribed requirements.
- 4.1.1 Component and material inspection. The contractor is responsible for insuring that components and materials used are manufactured, examined, and tested in accordance with referenced specifications and standards.
- 4.1.2 Disassembly inspection. Failure of any test by the first-produced model shall be cause for disassembly, in the presence of a Government representative, of the first-produced model to the extent necessary to determine the cause of the fuilure. Each disassembled part shall be examined in detail for compliance with this specification in regard to materials, dimensions, tolerances, and workmanship. Parts not complying with such requirements shall be rejected.
 - 4.2 Classification of inspection. Inspection shall be classified as follows:
 - a. First-produced radiator inspection (see 4.3).
 - b. Quality conformance inspection (see 4.4).
 - c. Inspection of packaging (see 4.6).
 - 4.3 First-produced radiator inspection.

- 4.3.1 Examination. The first-produced radiator(s) shell be examined as specified in 4.5.1. Presence of one or more defects shell be cause for rejection of all first-produced radiator(s).
- 4.3.2 Tests. The first-produced radiator(s) shall be tested as specified in 4.5.2.1 through 4.5.2.5. Failure of any test shall be cause for performing the inspection specified in 4.1.2.
 - 4.4 Quality conformance inspection.
- 4.4.1 Sampling. Sampling for examination and tests shall be in accordance with MIL-STD-105, Inspection Level II.
 - 4.4.2 Examination.

- 4.4.2.1 <u>Samples</u>. Samples selected in accordance with 4.4.1 shall be examined as specified in 4.5.1. AQL shall be 2.5 percent defective for major defects and 4 percent defective for minor defects.
 - 4.4.3 Tests.
- `4.4.3.1 Samples. Samples selected in accordance with 4.4.1 shall be tested as specified in 4.5.2.1 through 4.5.2.5. AQL shall be 2.5 percent defective for major defects and 4 percent defective for minor defects.
 - 4.5 Inspection procedure.
- 4.5.1 Examination. The radiators or cores shall be examined for the following defects:

Major

- 101. Dimensions not as specified.
- 102. Material not as specified.
- 103. Sering not as specified.
- 104. Priels are not corrosion resistant or treated to be made corrosion and istant for the applicable storage and operating environments.
- 105. Divainilar metals as defined in MIL-STD-889 are not effectively insulated from each other.
- 106. Contractor does not have documentation available for identification of material, material finishes, or treatments.

Minor

- 201. Identification marking incorrect or illegible.
- 202. Cleaning not as specified.
- 203. Workmanship not as specified.
- 4.5.2 Tests.

- 4.5.2.1 Conditions. The following conditions shall apply during the tests performed in accordance with thir specification on complete radiators and on radiator cores when they are fur hed separately. Radiator cores furnished separately shall be tested in fixtures which simulate, for test purposes, the top and bottom radiator tanks.
- 4.5.2.1.1 Supports. The radiator or core shall be supported on its normal points of support and shall not be supported on a cradle or bracket which in any way restrains the possible distortion of the radiator or core when under pressure.
- 4.5.2.1.2 Equipment. The test radiator or core, as applicable, shall be mounted on a test stand. A circulating pump shall be used to maintain an even temperature in the water reservoir. A flow pump and piping shall be used to provide water to the test radiator or core and a throttling valve shall be used to regulate the flow to the desired rate. A variable speed fan or adjustable dampeners or louvers shall regulate the sirflow to the test radiator or core.
- 4.5.2.1.3 <u>Instrumentation</u>. <u>Instrumentation shall be provided to perform the following functions:</u>
 - a. To measure the temperature in the waterline at inlet and outlet to test radiator or core
 - b. To measure airflow in the airduct. (When an orifice is used to measure the airflow, a manometer shall be connected upstream from the orifice to indicate the static pressure in the duct.)
 - c. To measure the pressure drop or the resistance to airflow across the core.
 - d. To measure the temperature of the airflow on each side of the core.
- 4.5.2.1.4 Control limits and data observations. The observed data shall be recorded. All points for each test shall be recorded only after all variables have been stabilized. The degree of stabilization and accuracy of observations shall be acceptable if the heat-rejection comparison conforms to 3.5.2.
 - 4.5.2.1.5 Coolant. The coolant shall be water.
- 4.5.2.1.5.1 Coolant temperatures. The temperature of the water entering the test section shall be between 170° F and 210° F.
- 4.5.2.1.6 Heat rejection. The heat rejection test shall be made using one of the following test methods.
- 4.5.2.1.6.1 Heat rejection, test method (a). The core section shall be tested in the wind tunnel at the 100 percent waterflow rate and at 125 percent of the rated waterflow. If these selected values are not possible the core shall be tested at not less than three waterflow rates which bracket the 100 and 125 percent rate for each radiator size. At each waterflow rate, the heat rejection shall be determined at not less than four air velocities overlapping the range of 1.500 to 2,100 feet per minute as indicated on sheet 7 of MS35773. The heat

rejected by the water and the heat gained by the air shall be separately calculated at each test condition. A performance curve shall be pibited as shown on MS35773, Figure 1 or 2, as applicable. The heat rejection and core remastance values at 1,500, 1,800, and 2,100 feet per minute air velocity shall be taken from the performance curve and recorded. The difference between the test danta and standard core data shall be checked for conformance to 3.5.1.

4.5.2.1.6.2 Beat rejection, alternate test method (b). When the same come section is used for more than one radiator type and size, waterflow rates and air-velocity rates which overlap the entire range of required conditions small be chosen for test points on the sample core. All the air velocities shall be tested at each chosen waterflow rate. These results shall be placed as abnown on MS35773, figure 1 or 2, as applicable. The varying waterflow rates in galilhous per minute can be plotted as a parameter on these curves. From these curves, a cross plot can be made with heat rejection in Btu/minute as the whinate, waterflow rates as the abscissa, and air velocity lines of 1,500, 1,800, and 2,100 feet per minute as the parameter. From this cross plot, the required values can be obtained and recorded. The data thus obtained shall be compared to the standard core values of MS35773, Figures 1 and 2, as applicable. The difference between the test data and standard core data shall be checked for conformance to 3.5.1.

4.5.2.1.7 Air flow. Air flow through the test core section stall be from either side.

4.5.2.1.8 Air-pressure-drop-corrections. The sir-pressure-drop measurements shall be corrected to standard conditions by use of the following formulas:

4.5.2.1.9 Vibration. The radiator shall be filled with tapwarm for the test specified in 4.5.2.4. The radiator shall be supported as specified in 4.5.2.1.1 and securely fastened to a rigid mounting bracket which shall be builted to the vibration table to insure that the motion of the radiator shall be essentially the same as the motion of the platform. Heans shall be provided for controlling the direction of vibration of the test machine and for adjusting and measuring frequencies and amplitudes of vibration to keep them within prescribed limits.

4.5.2.2 Heat rejection and core resistance. The radiator or core, as applicable, shall be tested as specified in 4.5.2.1.6 based on costed heat rejection as defined in 6.4.12. These values may be determined con a square-foot basis. These values shall then be corrected to the area in square feet. Nonconformance to 3.5.1 shall constitute failure of this test.

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4.5.2.3 Pressure cycling. The complete radiator shall be tested with all outlets closed. Pressure, variable from atmospheric to 150 percent of cap pressure not exceeding 18 psig, shall be applied at the inlet using air, steam or glycol and shall be maintained at a temperature of at least 212' F during the test. When steam is used, means shall be provided to prevent the accumulation of water. The pressure cycling shall take place in 3 to 4 seconds and at a rate of 6 pressure cycles plus or minus 1 cycle per minute. The radiator shall be cycled to a minimum of 50,000 pressure cycles. The radiator shall be examined periodically for evidence of leakage or distortion. Only tube leaks and tube-to-header leaks, not to exceed three, shall be repaired or plugged before continuing the test. Any evidence of leakage or maximum permanent distortion of more than 1/8 inch shall constitute failure of this test.

4.5.2.4 Vibration.

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4.5.2.4.1 Resonance survey. The radiator which has been tested in accordance with 4.5.2.3 may be rebuilt or another radiator may be used for this test. The radiator shall be tested for leakage prior to start of this test. The radiator shall be prepared in accordance with 4.5.2.1.9 and vibrated at frequencies from 10 cps to 33 cps at the table displacements specified in table I. The change in frequency shall be made at intervals of 1 cps and maintained at each frequency for 1 minute. If resonance occurs at any point in the specified range, the frequency of vibration at that point shall become the test condition for 4.5.2.4.2.

4.5.2.4.2 Procedure. This test shall be run after completion of 4.5.2:4.1 if no leaks are observed. The radiator shall be vibrated for not less than 24 hours at the most critical resonant frequency. If no resonance was observed, this test shall be performed at 33 cps at the displacement referenced in table I. The radiator shall be periodically examined during the test for evidence of seepage and leakage. Nonconformance to 3.5.4 shall constitute failure of this test.

Table I. Table Displacements.

quency range	Total table displacement
cps	inches
19 to 15	· · · 0.060 + 0.006
16 to 25	0.050 7 0.005
26 to 33	0.040 7 0.005

4.5.2.5 Washing operation. The radiator or core shall be filled with distilled water or tapwater of known pH index (see 6.4.13), at a temperature of 80° F to 100° F. The radiator shall then be shaken to assure thorough mixing and then allowed to stand for 1 hour. At the end of the 1-hour period, 1/2 gallon of the contents shall be drained into a clean container and tested for pH change and chloride content. Nonconformance to 3.10.1 shall constitute failure of this test.

- 4.6 Inspection of packaging.
- 4.6.1 Quality conformance inspection of pack.
- 4.6.1.1 Unit of product. For the purpose of inspection, a completed pack prepared for shipment shall be considered a unit of product.
- 4.6.1.2 Sampling. Sampling for examination shall be in accordance with HIL-STD-105.
- 4.6.1.3 Examination. Samples selected in accordance with 4.6.1.2 shall be examined for the following defects. AQL shall be 2.5 percent defective.
 - 104. Haterials, methods, or containers not as specified for level A or B. Each incorrect material, method or container shall constitute one defect.

 - 106. Gaskets not preserved as specified for level A.
 - 107. Contents not ismobilized within box as specified for level A.
 - 108. Box closure and sealing not as specified for level A.
 - 109. Radiators or replacement core-assemblies of unlike description packed together for level A or B.
 - 110. Quantities packed together exceed the weight limitation of the box fixed level A or B.
 - 111. Preservation or packing not in accordance with the referenced documents as specified for commercial.
 - 112. Marking missing, illegible, incorrect, or incomplete for level A, B or commercial.

5. PACKAGING

- 5.1 Preservation. Preservation shall be level A or commercial as specified (see 6.2).
- 5.1.1 Level A. Unless otherwise specified (see 6.2) radiators or replacement core-assemblies shall not require application of a contact preservative. When specified (see 6.2), slush or flush interior of radiators replacement core-assemblies with VV-L-800'to insure complete coverage and thoroughly drain excess. Openings into radiators or replacement core-assemblies shall be sealed with tape conforming to MIL-T-22085, Type II or with caps or plugs of the appropriate size conforming to MIL-C-5501. The filler neck cap shall be secured in place to prevent loss. Gaskets for each replaceable core assembly shall be protected with fiberboard stiffeners and shall be preserved in accordance with MIL-P-116, Method IC-1 or IC-3. Each radiator or each replaceable core-assembly with gaskets, shall then be placed in a close-fitting box conforming to PPP-B-636, class weather resistant, grade as applicable, style optional. The contents shall be blocked, braced or cushioned as applicable within the box two prevent movement or damage. Box closure and sealing shall be as specified first method V in the appendix to the box specification.

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 2.1.2 Commercial. Each rediator or replecement core-assembly with gaskets.
- shall be preserved in accordance with MIL-STD-1165.

 5.2 Packing. Packing shall be level A, level B or commercial as specified (see 6.2).
- 5.2.1 Level A. Ladistors of like description or replacement corr-assemblies -of like description, preserved as specified in 5.1, shall be packed together in a close-fitting box conforming to PTP-B-601, overseas type, style optional, in quantities not to exceed the weight limitation of the box. Box closure and strapping shall be in accordance with the appendig to the box specification. The second of the second of the second
- 5.2.2 Level B. Redictors or replacement core-assemblics with gaskets shall be packed, as specified in 5.2.1 for level A except that bexes shall be demestic type.
- The state of the s 5.2.3 Commercial. Radiators or replacement core-assemblies with gashets, preserved as specified in 5.1, shall be packed in accordance with MIL-STD-1188.
- 5.3 Marking.

 5.3.1 Military Marking for military levels of protection (level A or B)

 shall be in accordance with MIL-STD-129.
- 5.3.2 Commercial. Merking for commercial packaging shall be in accordance th MIL-SID-1188. 6. NOTES
- use with liquid-cooled internal combustion engines to dissipate the he from the coolant.
 - 6.2 Ordering data. Procurement documents should specify the following:
- a. Title, number, and date of this specification.
 - b. Date of issue of DoDISS applicable and exceptions thereto (see 2.1.1).
 - c. Type of radiator or core, when applicable, required (see 1.2).
- d. Time frame required for submission of first-produced radiator(s) and file - number of radiators required (see 3.2).
- When the Coverment will conduct may or all of the preproduction model e. When the Government will conduct some but not were the Covernment will conduct some but not were all of the preproduction examination and tests, the contracting officer should specify which examination and tests will be conducted by the Government and which examination and tosts shall be conducted by the contractor (see 3.2).
 - f. Finishing and painting when other than as specified (see 3.7).
 - g. Applicable MS part number required (see 3.8).
 - h. Applicable MS part number required (see 3.9).
 - i. Degree of preservation and degree of packing required (see 5.1 and 5.2).
 - j. When interior of radiator or replacement core-assemblies are to be preserved (see 5.1.1).

6.3 First-produced radiator. Any changes or deviations of production radiators and cores as applicable, from the approved first-produced radiator during production will be subject to the approval of the contracting officer. Approval of the first-produced radiator will not relieve the contractor of his obligation to furnish radiators and cores as applicable, conforming to this specification.

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- 6.4 Definitions. For the purpose of this specification, the following definitions shall apply.
- 6.4.1 Rated internal pressure. The rated internal pressure shall be 7 psig for radiators conforming to MS35773-1 through -10.
- 6.4.2 Standard air. Standard air shall be air at a temperature of 70° F, a barometric pressure of 29.92 inches of mercury, and a density of 0.075 pound per cubic foot.
 - 6.4.3 Rated sir velocity. The rated air velocities shall be those listed on sheet 7 of MS35773.
 - 6.4.4 Rated coolant flow. The rated coolant flow shall be the flow listed on sheet 7 of HS35773, and shall be based on approximately a 10° F drop in coolant temperature in the radiator.
 - 6.4.5 Heat transfer heat energy absorbed by air flow. The heat energy absorbed by air flow is the product of the air flow, specific heat of air, and air temperature rise.

Heat energy absorbed by air flow - WCp AT

w = air flow rate, Lba/Min.

Cp = 0.24 Btu/Lbm/°F

ΔT = air temp rise, "F

6.4.6 Heat transfer - the heat rejection from water flow. The heat rejection from water flow is the product of the coolant flow, specific heat of coolant and coolant temperature drop.

Heat transfer (heat rejection from water flow) = WCp AT

W - water flow rate, Lba/Min.

Cp = 1 Btu/Lbm/°F

△T = water temp drop, *F

6.4.7 Specific heat at constant pressure of water. The specific heat at constant pressure of water shall be based on the average water temperature. The

MIL-R-45306C specific beat at constant pressure shall have the value of 1 Stu/lb./° F for "

- water temperatured up to 215, 7.

 6.4.8 Specific best at constant pressure of air. The specific best at constant pressure of siz shall have the value of 0.24 Btu/lb./° 7 for air temperatures up to 215 F and pressure around 1 (atms).
 - 6.4.9 Average water temperature. The average water temperature of the radiator is the sum of the water inlet and outlet temperatures divided by 2.
 - 6.4.10 Rated potential. Rated potential shall be defined as the average water temperature minus the entering hir temperature and shall have a value of 50° F.
 - 6.4.11 Observed potential. Observed potential shall be defined as the observed average water temperature minus the observed entering air temperature during heat-rejection and core-resistance test.
 - 6.4.12. Rated best rejection. The rated heat rejection shall be total observed heat rejection in Biris per minute sultiplied by the rated potential and divided
 - by the observed potential.

 6.4.13 Index of acid intensity. The pH index shall be defined as the negative logarithm of the hydrogen ion concentration per liter. A pH index of 7 is a neutral solution. A pH index of less then 7 is an acidic solution. A pH index of greater than 7 is a basic solution.

 6.4.14 Resonance. Resonance is a condition of maximum magnification of an
- 6.4.14 'Resonance. Resonance is a committee of marketing of applied vibration of applied vibr the radiator under test
 - 6.5 Recycled material. It is encouraged that recycled material be used when : practical as long as it weets the requirements of the specification (see 3.3)

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Arby - ME

Air Force - 99

Review activity:

Army - AT

Air Force: 82

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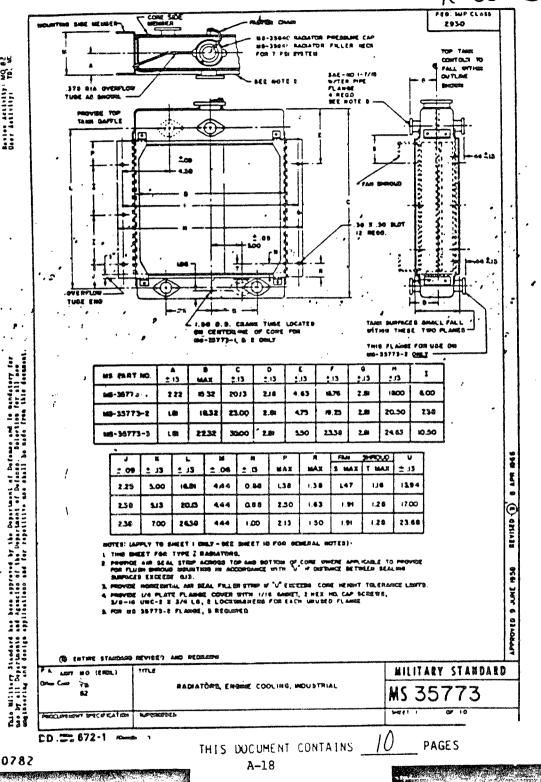
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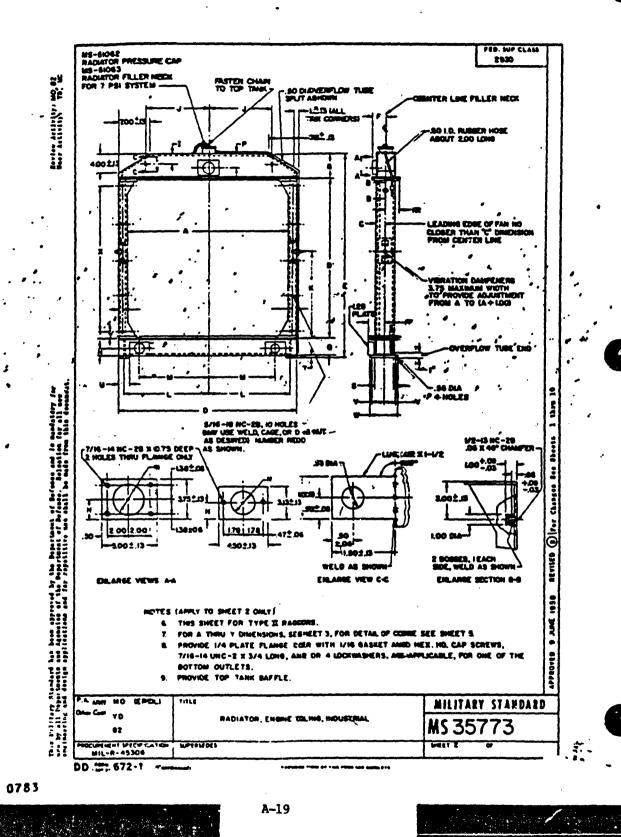
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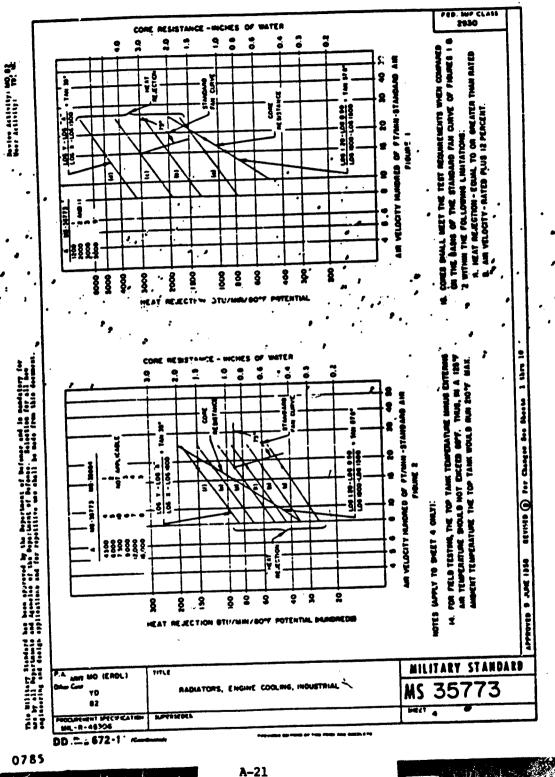




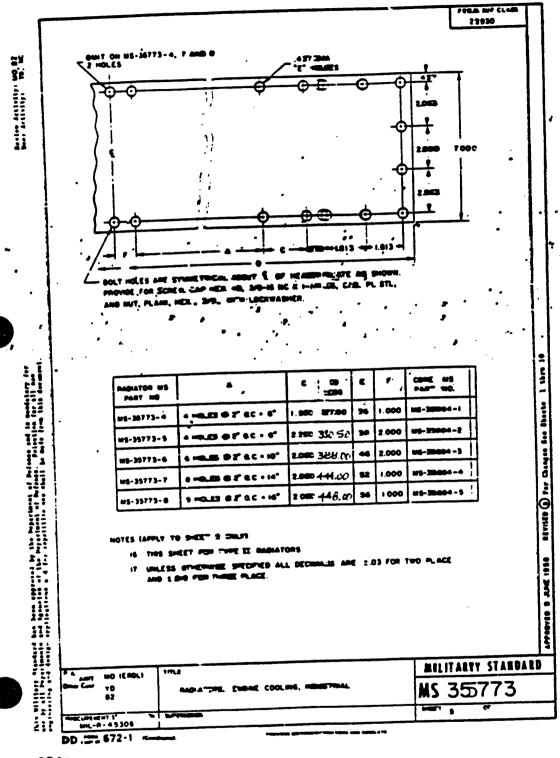
IR WE CLASS 5930 1.13 MS PART NO 2.04 1 13 2.13 2.13 2.18 **2.13** 2.13 **2.0** 2.04 34 38 12.75 MS-35773'→ 2350 27.00 2.38 2700 300 1.36 2.50 860 13.50 SEE NOTE II 39.30 SEE ROTE II 1.56 000 15.00 14.50 34 MS-35773-9 2700 2.30 30 50 3.00 20,00 47.00 18.00 15.50 2.34 600 1.60 12.00 33.50 36.00 38.00 MS-35773-4 SEE HOTE 12 2.34 20.00 MS-35773-7 39.50 40.00 4400 SEE MOTE 12 55.00 ક્રક . 12.00 MS:-35773-0 4350 44.00 4400 17.00 has been approved by the Principality of Pricess and 16 medalogy for and According of the Popularies of Pricess. Solveting for all have applications and for repression way shall be adde firm this decembed :09 . CORE MS PART NO. 2.13 :.00 4.04 :.0 :.13 : 13 2.04 2.13 :.13 : 13 G-33004-400 330 7.00 4-HOLES & # U.C.+ 24 1.50 9.50 2,00 2.50 4,75 0.30 1.50 . 300 2.30 730 4.75 0.34 1.50 3.00 7.00 -HOLES @ 9" 0.C+27 1.30 15-35004-2 1425 2.10 400 12 50 700 330 430 730 4.73 0.50 3.00 300 700 S-HOLES OF OC-32 2.00 ; 16.50 300 720 450 3.50 4.73 0.50 3.00 3.00 7.00 5-HOLES @ 9"0 C - 34 2.00 7.00 S-HOLES @ ICOC+40 2.00 WS-33664-9 100 3 30 430 350 4.73 050 3 00 3.00 (Dealles) MOTES: LAPPLY TO SHEET 3 ONLYS-ID. THIS SHEET FOR TYPE & RADIATORS. H. INCLUDES 38" THICK MOUNTING FOOT. IZ. MICLUSES SO" THICK MOUNTING FOOT IL SOTTOM OF SIDE SUPPORT TO CENTER LINE OF VIGRATION DAI PENER This Military Standard too by all hepartments orgineering and design TITLE MILITARY STANDARD MO (EROL) YD FADIATORS, ENGINE COOLING, INDUSTRIAL MS 35773 PROCUREMENT SPECIFICATION SUPERSONS DD . 5. 672-1 ~

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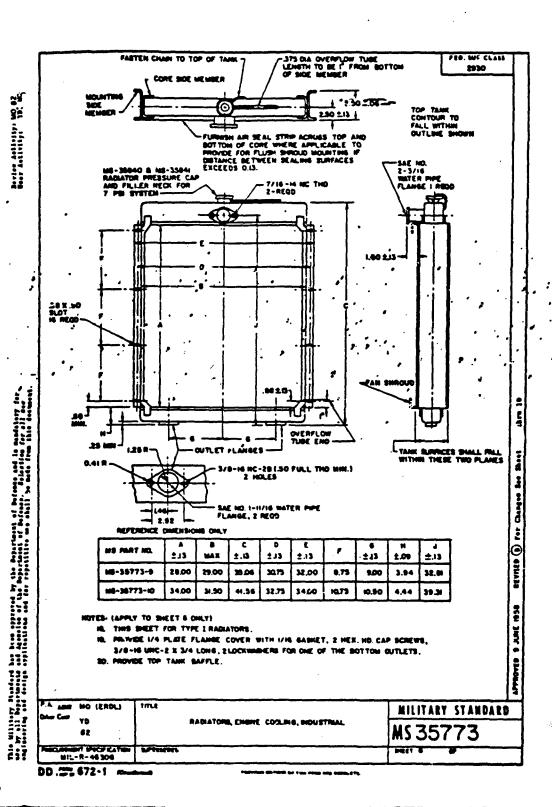


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HEAT MERCTION AND CORE RESISTANCE REGISTERENTS FOR MILITARY STANDARD RABIATORS MAX. REDISTANCE LEGINO HEAT REJECTION MR VELDCITY WATER FLOW WE PART SEE MOTE 21 STUMM ("A") FT/MIN MATED WALLE MONES WATER GAL SAME K RES ALLOW RATED VALUE • 1200 1363 WS-35773-4 1.2 2100 • 2000 2272 2531 1800 1800 2100 MS-36773-2 MS-35773-H •0.9 1.2 1(0) 23 1.5 Hel W-36773-3 . 3000 **** 40.0 36 3406 1.2 3797 * 8000 ' 9682 4328 M4-30773-0 62 3 1.2 1000 2100 *MS-35773-4 MS-35884-1 2000 4500 2(4) 2015 ME-35775-4 301 3281 9.9 94.**5**0 75 • 9000 ME-30004-5 , 1.5 3200 9400 240 16-35773-10 1800 •1800 •2100 40 92 * 7300 8369-1.8 7921 -9000 10080 M9-35773-4/ M9-36004-3 9.5 110 **...** 2106 1.5 WS-35773-7 210) 0.9 ~1.30 10560 .15000 12270 1.5 WS-26773-0 2111 13200 1000 -100 MG-35004-5 -19000 M710 200 LS

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HOTES (APPLY TO SHEET 7 CHLY);

- 21. REFER TO FIGURES AND CURVES WEET 4.
- 22. ABOVE REQUIREMENTS ARE BASED ON BOOF POTENTIAL.

SO'F POTENTIAL - MERANE WATER - ENTERING AND
MERANE WATER - T1 - T0- TANK TEMPERATURE, T2 - GOTTOM TANK TEMPERATURE

HEAT REJECTION CURVE . LOG Y - LOG "A" FOR X - FOR 4000 . LW 30.

RESISTANCE CURVE . LOS 120 - LOS 0.90 . TAN 97.6" LOS 1800- LOS 1500

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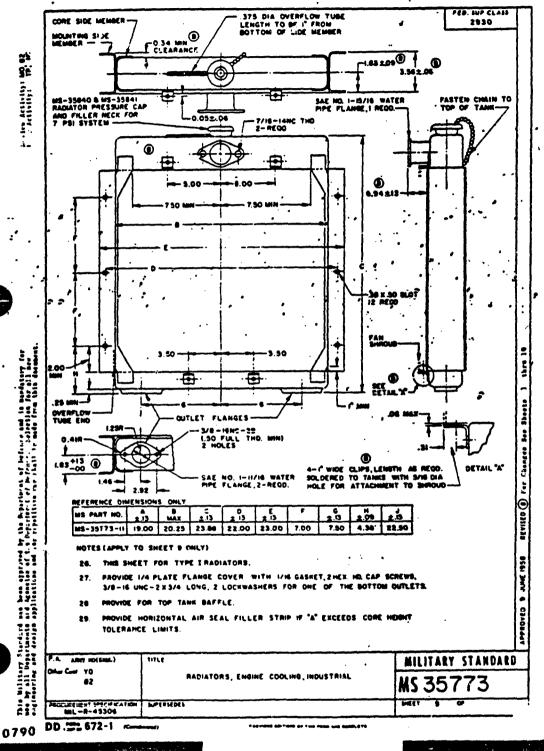
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2930 Der ine dettette 10, 02 MATERIAL REQUIREMENTS HEADER PLATES HEADER TANKS MACHATON BARS TUBE DO LIVE SIDES TYPE ISEE NOTE 23 TUBE WA ISEE WALL **80110M** tor NOTE 23 THE M\$ 35773-1 .004 1 **D00** 36773-2 1 ----206 2006 MS 36773-II 20 GA (D32) *16 GA. (.047) 20 CA (.032) *20 GA (D32) TERME WITH MASS . . 1 . M 14773-3 004 200 14 6A. (000) SAE IGIO WHIS ٠,١ n 35773-9 206 004 *18 CA (.040) 006 8 15773-IQ .006 BRASS MS 36773-4 MASS . تعند سان .006 006 ws 35004-1 10 GA (.135) *10 62 (J36) MS 36773-6 **SAE 1010 SAE 1010** 11 SAE :CIO 900 18 GA (1040) MS 35884-2 has been approved at the properties of the prope US 36773-6 ٥١٥, 11 SAE IOIO 200 P11 64 (.091) -MS 35884-3 BR/35 MS 39773-7 11 SAE 1010 7 CA 1 1771 *7 6A (177) 800 D10 for Changes See Sheats WS 35884-4 SAE 1010 SAE 1010 11 SAE IGIO .006 NOTES (APPLY TO SHEET & CHLT) 23 NOT APPLICABLE TO STANDARD US 35884 BEVISED (THE USE OF COPPER BEARING STEEL OR INGOT IRON IS ALLOWED IN PLACE OF SAE 1010 25. INTERNAL SURFACES OF PARTS CONSTRUCTED FROM SAE 1010 SHALL BE PROTECTIVE COATED. 26 GAGE SIZES SHOWN ARE MINHAUM APPROVED 9 JUNE 1938 the Military Standard age to by all Departments MINT MO LEROL MILITARY STANDARD T.L RADIATORS, ENGINE COOLING, INDUSTRIAL MS 35773 MII / PRODUCTION STOP EATE DD . 5. 672-1

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FEB. NUP CLASS 5930 Зe Boulos Artifeligi GENERAL NOTES LAPPLY TO SHEETS I THRU 91: iless otherwise specified, tolerances on decimal dimensions 1.03 inches. RADIATORS MS 35773-1 THRU MS 36773-41 WILL BE TESTED M WATER WITH AIR AT & LBS. MINIMUM TO IQ LBS. MAXIMUM PRESSURE. 32. ALL LIMENSIONS ARE IN MICHES. FOR DESIGN FEATURE PURPOSES, THIS DOCUMENT TAKES PRECEDENCE OVER PROCUREMENT DOCUMENTS REFERENCED HEREIN REFERENCED DOCUMENTS SMALL BE OF THE ISSUE IN EFFECT ON THE DATE OF INVITATIONS FOR BIOS. For Changes See Sheets 1 thru 10 This Military Standard has been approved by the Department of Defense and is mendatory for many all Properties and Agencies of the Department of Defense. Salestics for all new segmenering and design applications and for repositive use thall be made from this desiment (OSSIASE BEG! SHIFE & GSADEGEV 1 SHEET ADDED P.A. MINT MO (EROL) MILITARY STANDARD RADIATORS, ENGINE COOLING, INDUSTRIAL 35773 40 82 MS MIL-R-45306 10 DD . 25. 672-1 0791 A-27

APPENDIX B
M915 RADIATOR TEST RESULTS DATA

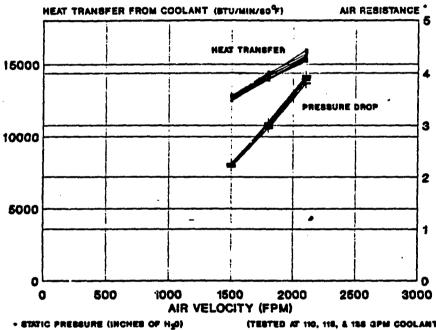
NOTES:

1. LEAKAGE:

THE RADIATOR, WITH ALL OPENINGS CLOSED, SHALL NOT LEAK IN EXCESS OF 5 CUBIC CENTIMETERS PER MINUTE, NOR FROM MORE THAN ONE LOCATION, WHEN SUBJECTED TO 18 + 1 PSIG AIR PRESSURE.

2. COOLING:

RADIATOR COOLING PERFORMANCE SHALL MEET REQUIREMENTS AS SHOWN IN GRAPH, WITH INLET WATER TEMPERATURE 180 ± 5 °F.



- (TESTED AT 110, 116, & 136 GPM COOLANT)
- 3. FILL RATE TEST: WITH RADIATOR OUTLET PLUGGED, THE TIME TO FILL THE RADIATOR TO 99% COOLING SYSTEM CAPACITY SHALL BE ACCOMPLISHED IN A 5 MINUTE PERIOD.
- 4. MAXIMUM FREE FLOW RATE TEST: WITH THE RADIATOR SUSPENDED BELOW A RECEIVING DRUM AND CONNECTED TO A COOLANT FLOW SYSTEM, THE MAXIMUM FREE FLOW RATE SHALL MEASURE 55 ± 5 GPM.
- 6. PRESSURE CAP: THE PRESSURE CAP SHALL MEASURE 10 PSIG.

- 7. FAILURE:
 FAILURE TO MEET NOTES 1 THROUGH 4 WILL
 RESULT IN FAILURE OF THE RADIATOR.
- 8. FINISH:
 PRIME TO BEST COMMERCIAL PRACTICE AND BE
 COMPATIBLE WITH MIL-E-52853A AND
 MIL-E-52798A. COLOR BLACK.
- 9. INTERNAL CLEANLINESS:
 THE RADIATOR ASSEMBLY SHALL BE CLEANED AND
 BE FREE OF DEFECTS AND FOREIGH MATERIAL.
 AFTER CLEANING, WATER FROM THE CLEANED
 RADIATOR SHALL NOT SHOW A "PH" CHANGE OF
 GREATER THAN 1, AND A CHLORIDE CONTENT
 INCREASE OF GREATER THAN 75 PARTS PER
 MILLION WHEN COMPARED TO THE INDUCED WATER.
- 10. REMOVE ALL BURRS AND SHARP EDGES.

NOTES 1,8,9, & 10 TAKEN FROM 5-TON TRUCK RADIATOR

Fill-Rate Test Results Time to Fill to 90% Capacity (in minutes)

Test Run	Radiator #1	Radiator #2
1	0:30	0:30
2	0:29	0:28
3	0:28	0:30
Average	0:29	0:29

Table B-1.

Maximum Free-Flow Rate Test (Gallons per Minute)

Test Run	Radiator #1	Radiator #2
1	50.1	58.9
2	71.7	59.1
3	42.2	47.5
4	65.3	63.1
5	41.7	58.9
6	45.8	58.7
Average	52.8	57.7

Table B-2.

TEST DATA: 6AVELE #1 WATER TEMP IN: 188°F +18° AIR TEMP IN: 186°F +18° DENSITY WATER (188°F): 0.8986 LB /CAL

MOTES.
ALL TEMPERTURES IN DECREES FAHRENHEIT
CORE RESISTANCE CORRECTED TO STD ATH CONDITIONS
*DATA POINTS OMITTED(GREATER THAN 52)

RESIST * H20	22.22	258 85	2	12.26	3.6.6	3.93	222	523	3.88
PERCENT P	22.33	1.92	6.6	6.14	1.21 6.63 4.69	2.33	7.14	8.98 9.85 9.85	3.22
HEAT REJ AIR ØTU/MIN/89°F)	12679.8 12673.4 12679.2	11920.1 13920.1 14285.6 1	15554.4	12572.5 12623.4 12738.7	14146.7	15512.6 15459.4	12940.6	14453.5 14464.0 14427.0	15789.8 15789.5 15975.1
HEAT REJ NOTER (BTU/HIN/80"F)	12642.6 12379.7 12377.9	13929.5	15621.1	12013.6	14165.7 14165.7 13517.7	15113.4 14996.1 15071.2	13141.2 13822.6 12616.4	14843.0 13978.2 14299.4	15643.4 15281.3 15908.3
HEAT REJ AIR (BTU/HIN)	13377.2 13117.6 12726.7	14241.0 13650.5 14241.0 15160.3	15282.2	13594.6	15468.8 15269.8 15139.8	15982.5 16104.0 16164.0	12965.2 12943.6 12986.2	14792.0 14662.8 14454.8	16873.0 16815.0 16664.0
HEAT NEJ NATER (BTU/HIN)	12017.9	14868.8 13926.8 13926.6	15347.7	12989.1 13161.5 13684.6	15281.3 15261.3 14421.7	15472.3 15567.8 15758.8	13256.2 13161.0 11978.9	14367.7 14179.4 14326.2	16593.8 16274.6 16594.3
ANE AIR TES-P	156.0 151.2 151.7	146.6 146.9 147.7	143.8	149.5 149.3 149.9	145	142.6 141.8 141.6	153.0 154.7 154.6	148.8 149.4 149.6	143.6 143.6 144.7
NE AIR TOS	22.2	91.9	93.7	8 8 8 8 8 8 8 8 8	85.5 86.1 87.1	96 68.0 68.4	94 95 95.1	91.9 93 94	88.3 69.8
TOO	166.3	165.7 165.1 165.1	163.8	166.3 166.3 166.3	164.2 164.4 166.9	163.8 163.7 163.0	168.9 176.1 169.5	167.5 167.9 167.9	166.2 166.3 166
TOTA TOTA	186.5	186.9	189.4	198.1 179.9 189	166.4	186	186.5	168 169.3 189.4	166.6 169.5 169.5
MIN FCON (CPS)	12375.0	14860.0	17367.6	12375.0 12375.0 12375.0	14839.8 14839.8 14839.6	17343.6	12375.6	14839.6	17325.0 17325.0 17325.0
MATTER PLOM (CPPH)	116.2	1169.8	911	115.5	2118	1111	137.6	138.4	136
TEST RUN	-44		M M	*****	# PA PA			~ M M	e

Table B-3. Heat-Rejection Data, Radiator Sample #1

FEST DATA: SAMPLE \$2 ISTER TEMP IN: 186°F +18° NIR TEMP IN: 186°F +18° DEMSITY WATER (180°F): 8.6986 LB /GAL

NOTES: ALL TEMPERATURES IN DECREES FAHRENHEIT CORE RESISTANCE CORRECTED TO STD ATH CONDITIONS *DATA POINTS OMITTED(GREATER THAN 5%)

RESIST HZO	222 232	2.95	3.8	22.2	2.96 2.95 2.95	3.82 3.86 3.86	2.28 2.19 2.19	2.96	3.88 3.89 3.87
PERCEAT DIFF.	2.57	6.97 2.38 1.72	1.71 3.39 8.98	6.47 . 1.76 1.29	6.51 1.88 1.17	2.65 8.39 2.37	12.39 2.64 9.37	1.31 2.86 2.48	8.41 1.91 8.73
HEAT REJ AIR BTU/HIN/80*F)	12491.7 14437.3 14445.5	13937.7 14628.4 14601.7	15375.3 15292.7 15346.7	12516.4 12528.5 12682.9	14022.7 14015.6 14060.5	15309.7 15306.4 15216.2	12729.5 12768.9 12755.7	14213.6 14188.2 14939.7	15524.5 15564.3 15509.8
HEAT REJ NATER (BTU/HIN/86°F)	12829.6 13777.7 14692.5	14074.9 14371.1 13766.9	15112.4 14774.8 15281.6	12575.6 12396.0	14894.6 13752.2 13896.4	15247.2	11152.8 12449.3 11561.8	14481.9 13896.6 14384.6	15461.6 15266.6 15624.2
HEAT REJ AIR (BTU/HIM)	12444.9 12531.6 12336.5	13685.0 13555.0 13502.9	14539.3 14568.9 14387.5	12943.6	14075.3	1463#.3 15449.9 1535#.#	12856.8 12986.9 12986.9	14231.4 14179.4 14205.4	16887.3 16148.8 15723.1
HEAT REJ MATER (BTU/HIN)	11959.0	13886.8 13886.8 13278.6	1429@.7 14617.6 14251.5	13157.2 12713.6 13134.3	14147.5 13657.7 13785.3	14243.1 15398.2 15731.4	11264.3 12721.7 11778.6	14419.9 13887.9 14555.4	16022.1 15039.1 15839.1
NVE AIR TENE OUT	151.4	147.6	144.7 144.9 145.4	156.4 156.7 156.6	147.1	144.9 143.1 142.6	153.4	148.7 148.5 147.5	163.4 163.3 164.1
AVE AIR TEMP	222	2 % C	96.6 97.1	* # # #	aa j	22.7	<u> </u>	325	96.4
WATER TOO	166.5 167.4 166.9	165.7 165.7 166	164.6 165.3 165.2	166.8	165.9 166.3 166	164.9	176 169.2 169.3	167.8 167.9 167.5	166.3 166.2 166.5
Maten Town NI	100.9	181.1 186.9 186.5	186.3 186.7 188.8	100.0	186.7 189.6 188.4	181	179.8 186.3 179.6	186.4 166 186.2	186.3 186 186.3
AIR (CM)	12375.0 12375.0 12375.0	14859.0 14859.0 14859.0	17325.0 17325.0 17325.0	12375.0 12375.0 12375.0	14859.6 14859.6 14858.0	17325.0 17325.0 17325.0	12375.6 12375.8 12375.6	14859.6 14859.6 14858.0	17325.6 17325.9 17325.8
MATER FLOW (GPM)	119.2	116.2	189.6	114.8	115.1 115 114.6	115.1	138.4	137.8	136.2
TEST ROW	-44.0	≠ 66 PA	# 19 19	# RI PO	- MM	- 17 P	4 4		# 19 M

Table B-4. Heat-Rejection Data, Radiator Sample #2

BELVOIR FUELS AND LUBRICANTS RESEARCH FACILITY (SWRI) 6220 CULEBRA ROAD - P.O.DRAWER 20010 PH:512-601-5111 SAN ANTONIO, TEXAS 78224

BFLRF

File: 02-1955-180 21 August 1990

Commander

U.S. Army Tank-Automotive Command Attn: AMSTA-RGT (Ms. Christine Radlein)

Warren, Michigan 48397-5000

ubject: Analysis of Fluids Drained From Radiators

Dear Sir:

Two fluid samples were received from TACOM for analysis. BFLRF was asked to identify the fluids if possible. The samples received were:

AL-19294-X Sample A, From Radiator No. 1 AL-19295-X Sample B, From Radiator No. 2

Since the two samples were expected to be the same with the exception of water in AL-19294-X, only AL-19295-X was analyzed. The sample was analyzed by gas chromatography and infrared spectroscopy.

A simulated distillation, using gas chromatography, was conducted on Sample AL-19295-X along with two known samples for comparison. The two known samples were a transmission fluid and a light machine oil (Singer Sewing Machine Oil). The chromatograms are given in Figures 1 through 3. Sample AL-19295-X is nearly identical in boiling point distribution to the two known samples, indicating that it is most likely a light weight (approximately 10 weight) oil such as a transmission fluid.

Figure 4 is the infrared (IR) spectra for Sample AL-19295-X. The peaks at 2920 cm⁻¹, 1460 cm⁻¹, and 1380 cm⁻¹ are consistent with the peaks from C-H groups. The other minor peaks are most likely due to trace contaminants or additives. The peak at approximately 3420 cm⁻¹ is due to water in the sample.

AMSTA-RGT (Ms. Christine Radlein) U.S. Army Tank-Automotive Command 21 August 1990 Page 2

In conclusion, the data indicate that the fluids received from TACOM are some type of light weight oil. If there are any questions concerning the analyses, please contact Steve Westbrook at (512) 522-3185.

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Very truly yours,

S.J. Lestz, Director

S.R. Westbrook Senior Research Scientist

SJL/SRW/lap (SRW.BB)

cf: U.S. Army Belvoir Research, Development and Engineering Center, Attn: STRBE-VF, Messrs. M.E. LePera and T.C. Bowen Belvoir Fuels and Lubricants Research Facility (SwRI), Attn: Mr. L.L. Stavinoha

Figure 1. GC Simulated Distillation of Sample AL-19295-X

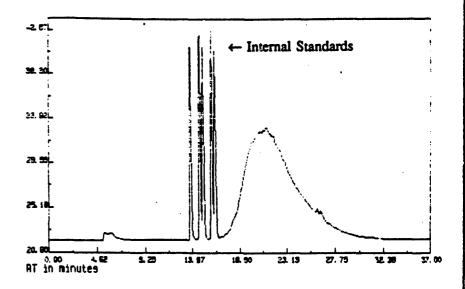


Figure 2. GC Simulated Distillation of Automatic Transmission Fluid

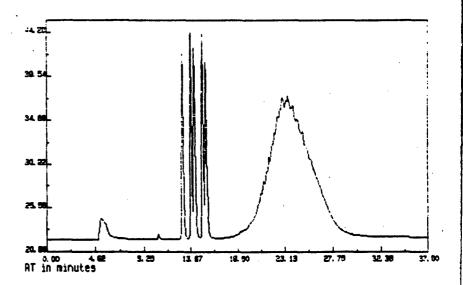
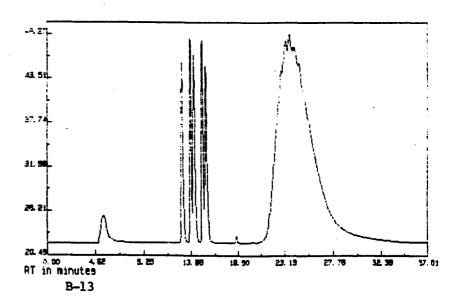


Figure 3. GC Simulated
Distillation of Light
Machine Oil



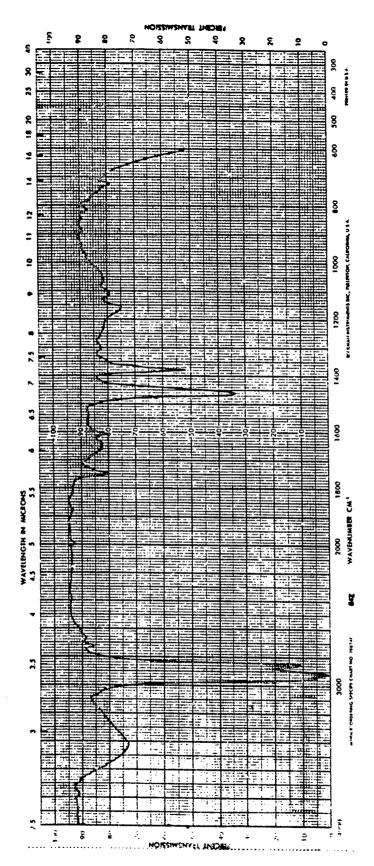


Figure 4. IR Spectra for Sample AL-19295-X

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